ESTABLISHING DRIVEWAY GRADES FOR NEW JERSEY HIGHWAYS

Volume I - Model Development

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by

Shahid Iqbal, Ph.D., P.E.

Gene Reilly

Wu Sun, Ph.D.

and

Louis J. Pignataro, Ph.D., P.E. Executive Director

The National Center for Transportation and Industrial Productivity
Institute for Transportation
New Jersey Institute of Technology
Newark, New Jersey



NJDOT Research Project Manager Robert Sasor

In Cooperation with
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and
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16. Abstract

Currently, the New Jersey Department of Transportation standards for state highway driveway grades are based on American Association of State Highway and Transportation Officials (AASHTO) guidelines, which are based on engineering judgements rather than research. The design of driveways is of great importance in terms of both safety and capacity of the roadway and the driveway. This study was conducted to reevaluate the AASHTO standards by attempting to safely extend the permissible grades for driveways.

The following objectives were addressed by the study:

- develop more liberal design standards than those in current practice
- develop new driveway grade standards based on computer simulation.

A twofold approach was designed for the study.

- In the first volume of the two volume report (Volume I- Model Development), a computer simulation model was developed and applied to assist an engineer in selecting a driveway profile starting from the outside edge of the main roadway. The application of this approach is suggested for driveways in excess of 50' in length. The AutoCAD simulation model (AutoDrive) has five modules:
 - 1. Input Module allows user to enter input variables
 - 2. Roadway Module draws roadway based on input variables
 - 3. Driveway Module draws driveway grades and inserts vertical curves
 - 4. Simulation Module places the design vehicle on driveway and performs simulation
 - 5. Output Module computes critical design parameters and displays results.
- In the second volume of the report (Volume II-Sight Distance Standards), the engineer is offered limiting sight distances based on a passenger car both on the mainline and at the driveway entrance. This approach is suggested for driveways of any length, in conjunction with the Input Variables for the Model, found in Volume 1.

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EXECUTIVE SUMMARY

Introduction

Currently, the New Jersey Department of Transportation's standards for State highway driveway grades are based on American Association of State Highway and Transportation Officials(AASHTO) guidelines, which are based on engineering judgements rather than research. The design of driveways is of great importance in terms of both safety and capacity of the roadway and the driveway. This study was conducted to reevaluate the AASHTO standards by attempting to extend the permissible grades for driveways.

Objectives

The following issues are some of those that the study addresses.

- determine the possibility of developing more liberal design standards than those in current practice, and
- develop new driveway grade standards based on data collected throughout the U.S. and by computer simulation.

Volume I – Design for the Simulation Model

The basic approach to the study is the development and application of a computer simulation model to assist an engineer in selecting a driveway profile starting from the outside edge of the main roadway. The AutoCAD simulation model (AutoDRIVE) has five modules:

- 1. Input Module allows user to enter input variables
- 2. Roadway Module draws roadway based on input variables
- 3. Driveway Module draws driveway grades and inserts vertical curves
- 4. Simulation Module places the design vehicle on driveway and performs simulation
- 5. Output Module computes critical design parameters and displays results.

The Input Module prompts the user to enter the following parameters:

- Design vehicle,
- Entering/initial speed (U) of the design vehicle,
- Minimum allowable speed on upgrades,
- Physical elements of roadway,
- Physical elements of roadway shoulder and driveway,
- Lengths of driveway vertical curves

In the Roadway Module, the following functions are performed:

- Set the drawing limits,
- Draw the roadway

In the Driveway Module, the following functions are performed:

- Draw the driveway surface,
- Place the design vehicle on the driveway surfaceIn the Simulation Module, the following functions are performed:
- Move the vehicle,
- Check appropriateness of cross-over, departure, and approach angles,
- Check for minimum standards,
- Check appropriateness of stopping sight distance

Simulation Model

AutoDRIVE is a 3D CAD based program that simulates the movement of selected design vehicle on the driveway profile. The program was developed using AutoLISP programming language, and it is written in DOS text using a suitable text editor. AutoDRIVE operates in AutoCAD environment and can be run on a personal computer (PC). The step by step instructions for using and installing AutoDRIVE on a PC are given in the manuals in the appendix. Users are allowed to enter design vehicle types, design vehicle dimensions, initial vehicle speed, and minimum speed. Although AASHTO lists several design vehicle types, there are practical limits in measuring clearances on vehicles. A field study was conducted to obtain clearance information. The vehicle operation characteristics on grades are governed by a vehicle speed-loss formula proposed by Thomas Gillespie (18), which follows.

 $DU/dX = 0.465[375(P/W)/U-G_r]g/U$

where, U = initial vehicle speed, or speed of vehicle entering grade (mph)

X = distance (ft)

 G_r = road grade (percent/100)

g = gravitational constant (32.2 ft/sec^2)

P/W = ratio of drive horsepower to vehicle weight

At the end of the program run, the model checks appropriateness of cross-over, departure, and approach angles, minimum standards, (such as minimum speed), and the appropriateness of stopping sight distance by advancing the vehicle. The major outputs of the simulation module include:

- Simulated speed at the end of Grade 1 (Km/h) (converted to km/h)
- Simulated speed at the end of Grade 2 (Km/h) (converted to km/h)
- Maximum allowable approach angle (degrees)
- Maximum allowable cross-over angle (degrees)
- Maximum allowable departure angle (degrees)
- Grade combination approach/departure angle (degrees)
- Grade combination cross-over angle (degrees)
- Stopping sight distance required (m)
- Length of curve between G1 & G2 is OK (Y/N)
- Length of curve between shoulder & G1 is OK (Y/N)
- Length of curve between G2 & property elev. Grade is OK (Y/N)

- Grade 1 is OK (Y/N)
- Grade 2 is OK (Y/N)
- Length of Grade 1 is OK (Y/N)
- Length of Grade 2 is OK (Y/N)

Vertical Curve Design

This study incorporates symmetrical parabolic vertical curves for the driveways to achieve better safety and comfortable operations on the grades. The design of vertical curves follows the AASHTO standards.

Sample Designs

Two design examples illustrate how the guidelines, methodologies, and models can be used in designing and evaluating the vertical alignment of driveways.

Volume II – Sight Distance Standards

This research effort has been designed to achieve the following objectives:

- Determine and develop the design standards that ensure safe sight distance for vehicles entering a driveway from the main line and for vehicles exiting from the driveway onto the major road, for the most critical conditions.
- Determine the possibility of developing more liberal design standards when the
 above mentioned situations are complicated by adverse combinations of
 curvatures and grades. This usually happens with either the main road or the
 driveway, or when there are lateral obstructions along the main road that can
 cause severe reduction in the sight distance from the main road to the driveway
 or vice versa.

The second volume discusses the minimum sight distance design requirements for passenger cars on the mainline and the driveway. Case studies and resulting tables are presented for perpendicular driveway alignments and for a range of driveway vertical grades (not to exceed a crossover grade of 9.4% as noted in Table 2.2 of Volume 1).

Future Research

In future studies, the following issues need to be addressed:

- Beside perpendicular driveways, the issues related to the combination of horizontal curves and grades need to be considered, because some driveways do not proceed perpendicular from the edge of the main road to the property.
- In this study the design of vertical curves on grades follows the AASHTO standards, which is suitable only for regular roadways. In future studies, a vertical curve design should be established specifically for driveways.

- The cross-over, approach and departure angles of a moving vehicle are significantly different from those of a stopped vehicle. In future studies, moving vehicle suspensions need to be included in the checking stage of the program.
- The current simulation model is an iterative procedure. In future studies, it could be upgraded to an optimization procedure to help engineers and transportation planners in their decision-making regarding driveway design.

1. INTRODUCTION AND STUDY PURPOSE

1.1 Study Problem

Currently, the New Jersey Department of Transportation (NJDOT) standards for State highway driveway grades are based on American Association of State Highway Officials (AASHTO) guidelines, which were developed in 1959. The AASHTO driveway grade standards are not supported by research and were probably based on the best engineering judgement at the time they were developed. Therefore, there is a need for reevaluation of those standards based on modern traffic and vehicle conditions and sight distance requirements.

The design of safe driveways encompasses many elements, namely, spacing, volume, use of property, angle of exit and entry, alignment, grade and superelevation of the highway and grade of the driveway. The importance of considering these elements in the driveway design would be reflected in the safety and capacity of the roadway and the driveway. As will be noted in the literature review there have been several studies, and some statements of practice, providing guidelines for various design factors. The use of the term "guidelines" concedes the potential for situations that are beyond those ordinarily encountered.

There are occasions when an increase, beyond the accepted guidelines, in the positive or negative grade of a driveway, would considerably reduce the cost of providing driveway access to the land parcel. It is further noted that most driveways are short in length and would cause vertical curve problems because of this small length ⁽¹⁾. It is because of these situations that the current study was conducted.

1.2 Study Objective

The research effort has been designed to:

- determine the possibility of developing more liberal design standards than those in current practice, and
- develop new driveway grade standards based on data collected throughout the U.S. and by computer simulation.

Two distinct and separate approaches to the problem were developed. The first volume of the two volume report details the development and use of a simulation model. The model development includes information on vehicle design, vehicle dimensions, vehicle operating characteristics on grade, and a vehicle's initial and minimum speeds on grade.

The second volume details the design requirements for the minimum sight distance for passenger cars on the mainline and the driveway. Case studies and resulting tables are presented for perpendicular alignments, a crest curve, and three mainline horizontal curves.

1.3 Literature Review

Several studies have been conducted addressing the design elements for driveways. The following reviewed literature briefly summarizes the most relevant articles. But as can be seen in the review, scant information is available on the development of the recommended grades for driveways.

The importance of proper driveway design is highlighted by the accident involvement of vehicles related to the driveways. In an early study ⁽²⁾, researchers simulated driving conditions for run-off-the-road accidents. Using specific embankment and back slopes, they concluded that a) driveway slopes present a roadside hazard, and b) the most cost effective driveway slope design standard is 8:1 (or 12.5%).

In a study of roadways in Texas ⁽³⁾, a significant number of accidents were found to be related to driveways; 10% of the total accidents on the state highway system and 16% of off-system accidents were in this category. The authors did not attempt to isolate the reasons for the accidents, except that they were related to driveways.

In an effort to provide access control guidelines to the Virginia DOT, the University of Virginia developed a methodology for commercial driveway spacing based on safety and level of service ⁽⁴⁾. But driveway profile was not included as one of the parameters in the model.

New Jersey Institute of Technology (NJIT) conducted a study of the relationship of driveways to accidents in New Jersey ⁽⁵⁾. It was found that "Approximately 30% of the reported accidents were midblock section accidents, which were primarily caused due to the presence of access points... Midblock section accidents were mainly caused by vehicles entering and exiting midblock access points."

In 1970, Texas A&M conducted a study for the National Cooperative Highway Research Program (NCHRP) ⁽⁶⁾ to develop guidelines for access control on major roadways. They state that "Access control ... insures that an arterial ... will continue to have a high traffic movement capability in future years." The states of Washington and Wisconsin were found to have made the most advances in implementing access controls on a system-wide basis. Although no specific limitations on grade are offered, grade change generalizations are made as follows:

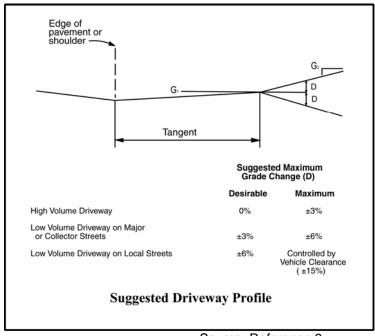
- "... standards ... would be in terms of performance or smoothness, but sufficient data relating driveway profile to smoothness and acceptable vehicle speed are not available..."
- "Where severe topography requires extreme grade changes, their undesirable effects can be largely offset by connecting the tangents with vertical curves. ... the desired length of curve (should be) ... approximately the wheel base of a passenger vehicle..."

 For low volume driveways, the maximum change (without using vertical curves) is 6% for arterial and collector streets, and a maximum change controlled by vertical clearance for local streets.

Another study "evaluated the effects of driveway width, curb return radius, and offset taper approach treatments on the speed and path of drivers entering and leaving driveways ..." ⁽⁷⁾. However, the studies were conducted on level terrain, without the added benefit of other traffic.

A 1983 study ⁽⁸⁾ on access control stated that "Driveway profile is a critical element of driveway design. It influences the speed and path of driveway users and therefore affects driveway operation and safety." General profile guidelines were offered by the authors.

The Institute for Transportation Engineers issued guidelines in 1987 (9) that included suggestions for driveway grades. It is recommended that exceeding the suggested grade changes should be accompanied by vertical curves. The importance of driveway profile design is justified from three aspects, including safety, comfort of vehicle occupants, and potential damage of the underside of vehicles. The report states that "Maximum grades are established by the physical dimensions of vehicles (principally wheelbase) and braking capacities, primarily of trucks. Designs must then be further refined as to: a) curb and shoulder cross-section within the right-of-way, and b) whether a sag or crest curve is required to complete the driveway beyond the right-of-way." The report suggests maximum grades for three classes of driveways, which are show in Figure 1.1. Suggested maximum grades for residential, and commercial and industrial driveways are 15 percent, and 5 to 8 percent, respectively. Driveway grades are recommended to be limited to 6 percent within 10 feet of the roadway edge. The driveway slope upward from the gutter line is suggested to be at least 10 feet and 40 feet long for residential and commercial driveways, respectively. For abrupt grade changes, vertical curves are recommended to connect tangents.



Source: Reference 9

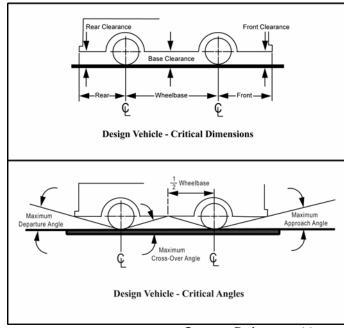
Figure 1.1 Suggested Driveway Profile

Although a 1988 review of driveway regulation practices does not list driveway grade in the general contents of a regulation for design standards, it does suggest that "The design elements of each high-volume driveway ..., and grades should be based on expected volumes by direction of arrival, and by vehicle characteristics" (10).

A 1991 Texas study of guidelines for vertical alignment of driveways lists four general engineering considerations that should be considered in the design:

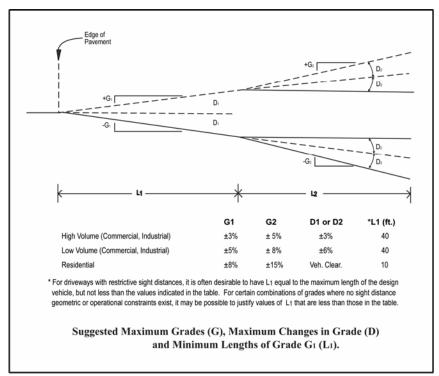
- human factors for driver ability and driver comfort,
- traffic characteristics for volumes, speed, vehicle type and accidents,
- physical elements for geometric design, traffic control and intersection location, and
- economic factors for direct and indirect costs.

For engineering design they further list four specific design elements: area type (rural, urban, suburban), driveway classification (residential, public, commercial, industrial), streets and highways (arterials, collectors, local), and design vehicle (length, clearances, wheelbase). The critical dimensions and angles for a design vehicle are shown in Figure 1.2. The authors conclude that if minimum guidelines cannot be followed, as outlined in the Federal Highway Administration (FHWA) publication Access Management for Streets and Highways, and illustrated in Figure 1.3, "adjustments should be made using engineering judgment (11)."



Source: Reference 11

Figure 1.2 Critical Dimensions and Angles of Design Vehicle



Source: Reference 11

Figure 1.3 Guidelines for Grade Design

The 1992 NCHRP study ⁽¹²⁾ on access management for activity centers qualifies the guidelines outlined in the FHWA publication. "Driveways vary widely in their design requirements. A driveway leading to a single residence is usually a simple curb cut that is limited in size. Conversely, a driveway leading to a major activity center, a shopping center, or a corporate office park is really an arterial street and must be designed as such." The initial grade for a driveway is predicated on the existence of a curb. The recommendation for subsequent grades are similar to those suggested above.

One of the most recent publications on the subject of access management was developed by the Transportation Research Board Committee on Access Management ⁽¹³⁾. It is a comprehensive synopsis of the findings and engineering judgments to date governing spacing practices. But specific guidelines are not suggested for the profiles of driveways.

The FHWA developed an NHI course ⁽¹⁴⁾ on access management in 1991. A compelling safety argument for the careful design of driveways is found in section 3.4.1, Vehicles Traveling Slower Than the Average Speed of Traffic Are More Likely to be Involved in a Crash. It was shown that the relative crash rates increased exponentially with speed differential. Section 3.9.2 relates the vertical alignment of driveways to the functional classification of the roadway, recommending 15% as the maximum grade on minor collectors and local roads.

The New Jersey Department of Transportation (NJDOT) State Highway Access Management Code ⁽¹⁵⁾ gives guidelines for driveway profile controls under subchapter 16:47-3.8, "Access point control dimensions for streets and driveways." The basis for these guidelines was the 1959 American Association of State Highway and Transportation Officials (AASHTO) standards, which were not substantiated by empirical data.

2. STUDY DESIGN

2.1 Introduction

The nature of the study requires an explanation of several aspects of both the study design and expected output. The two basic approaches to the study are the determination of the limiting sight distances on the mainline and driveway for passenger cars (volume 2), and the development and application of a computer simulation model to assist an engineer in selecting a driveway profile starting from the outside edge of the main roadway (volume 1). This section of the report will explain the steps and input in the modeling process and provide background details for the procedure. As further background, a limited number of interviews were conducted with State, Federal, and academic professionals to receive their views on the limits to design standards ⁽¹⁶⁾. A list of those interviews is in Appendix A.

2.2 Procedure for Model Development

The AutoCAD simulation model (AutoDRIVE) has five modules. These modules are listed below based on the type of function each module performs:

- Input Module allows user to enter input variables
- Roadway Module draws roadway based on input variables
- Driveway Module draws driveway grades and inserts vertical curves
- Simulation Module places the design vehicle on driveway and performs simulation
- Output Module computes critical design parameters and displays results

2.3 Selection of Input Variables for Model

2.3.1 Design Vehicle

Design vehicles (DV) are selected motor vehicles with dimensions, operating characteristics, and weight used to establish driveway design controls for accommodating vehicles of designated classes.

The largest of all the several design vehicles are usually accommodated in the design of highways. For design of driveways, selection of design vehicle will be based on: a) type of driveway (e.g., passenger car for residential driveway, SU/WB-12/WB-18 for commercial or industrial driveway), b) physical dimensions and operating characteristics of the vehicle.

The current version of AutoDRIVE model allows selection of design vehicle from the following three general classes (based on AASHTO Green Book):

- 1. Passenger cars (P)
- 2. Trucks
 - Single-unit truck (SU)

- Truck intermediate semitrailer combination (WB-12)
- Truck large semitrailers combination (WB-15)
- Truck double bottom semitrailer/full trailer combination (WB-18)

3. Bus

• Single unit bus (BUS)

2.3.2 <u>Design Vehicle Dimensions</u>

The physical dimensions of a design vehicle (see Figure 1.2) include:

- Height Height of vehicle measured from roadway surface to the roof of vehicle, in meters.
- 2. Length Overall bumper-to-bumper length of vehicle, in meters.
- **3.** Front Overhang Length, in meters, from the front edge of vehicle's front bumper to the center of its front axle.
- **4.** Rear Overhang Length, in meters, from center of the vehicle's rear axle to the edge of the rear bumper.
- **5.** Wheelbase Length, in meters, from center of the vehicle's front axle to center of its rear axle.
- **6.** Front, Rear, Base Clearances Vertical height, in meters, between roadway surface and low point of the front, rear, and base of vehicle, respectively.
- **7.** Approach, Departure, and Cross-Over Angles Approach and departure angles are used to determine critical sag grade breaks, and cross-over angles are used to determine critical crest grade breaks (see Figure 1.2).

Although AASHTO lists several design vehicle types, there are practical limits in measuring clearances on vehicles and on the classification of vehicles using driveways. Each of the vehicle types considered in the study are defined by the P/W ratios (see Section 2.3.3.2), and by the following critical dimensions and angles referred to in Figure 1.2. All dimensions in Table 2.1 are shown in meters. The dimensions were taken from field measurements, and are listed in the Appendix C.

Table 2.1 Vehicle Dimensions

Design	Criteria		Vehicle Type					
			PC	SU	TT	Bus		
Wheelba	ase		2.32-3.11	3.41-5.55	6.83-	N/A		
					11.59			
Base Cl	earance		0.18-0.37	0.21-0.58	0.46-0.85	N/A		
Front Cl	earance		0.18-0.52	N/A	N/A	N/A		
Rear Cle	earance		0.24-0.46	0.30-0.49	N/A	N/A		
Front O	/erhang		0.73-1.28	N/A	N/A	N/A		
Rear Ov	erhang		0.61-1.43	1.83-2.68	N/A	N/A		
Max.	App.	Grade	18%	N/A	N/A	8.3%		
Change								
Max.	Dep.	Grade	16%	16%	N/A	7.6%		
Change								
Max. Cr	ossover (Grade	12.5%	12.5%	13%	10%		

To include the impact of the dynamics of a vehicle's suspension on the points of vertical intersection of the driveways, the grade change maximum values are reduced by a factor of 0.75 and shown in Table 2.2.

Table 2.2 Maximum Grade Changes

Design Criteria			Vehicle Type				
			PC	SU	TT	Bus	
Max.	Dep./Appro.	Grade	12%	12%	N/A	7.6%	
Change							
Max. Crossover Grade			9.4%	9.4%	9.8%	10%	

The AutoDRIVE simulation model uses the default dimensions as shown in Table 2.1 (based on Table II-1 of the AASHTO Green Book and NJIT field survey). The model allows the user to edit/modify these dimensions.

Table 2.3 Default Vehicle Dimensions in Simulation Model

Table 216 Delatit Verricle Diritatione in Chinalation Medici										
Design			OVERHANG		WHEELBASE		CLEARANCE			
Vehicle	Heigh	Length	Front	Rea	WB1	WB2	WB	Front	Rear	Base
	t			r			3			
Р	1.3	5.8	0.9	1.5	3.4			0.30	0.30	0.30
SU	4.1	9.1	1.2	1.8	6.1			0.37	0.37	0.37
BUS	4.1	12.1	2.1	2.4	7.6			0.40	0.40	0.40
WB-12	4.1	15.2	1.2	1.8	4.0	8.2		0.40	0.45	0.45
WB-15	4.1	16.7	0.9	0.6	6.1	9.1		0.40	0.45	0.45
WB-18	4.1	19.9	0.6	0.9	3.0	6.1	6.4	0.40	0.45	0.45

Source: Reference 17

Note: Vehicle clearances are based on field measurements by NJIT (see Appendix C)

2.3.3 <u>Design Vehicle Operating Characteristics on Grades</u>

2.3.3.1 Vehicle Speed-Loss Formula on Grades

The following formula offered by Thomas Gillespie ⁽¹⁸⁾ combines the power/weight ratio of vehicles, the initial vehicle speed, and the roadway grade to calculate the speed loss per foot of a vehicle.

 $DU/dX = 0.465[375(P/W)/U-G_r]g/U$

where, U = initial vehicle speed, or speed of vehicle entering grade (mph)

X = distance (ft)

 G_r = road grade (percent/100)

g = gravitational constant (32.2 ft/sec^2)

P/W = ratio of drive horsepower to vehicle weight

The loss of speed is a necessary calculation for vehicles to ensure that the vehicle's speed is not reduced below a predetermined (minimum) level. On driveways, the lowest level of speed that a vehicle can reach (minimum speed) can be considerably less than that which is permitted on the main road. A later discussion of the minimum speed offers suggestions on an acceptable level.

To establish the maximum grade of a driveway, there are three inputs that must be determined for the speed-loss equation, the P/W ratio for each class of vehicle, the initial speed of the vehicle, and the maximum allowable speed loss on the grade. The minimum speed of the vehicle on the grade will set a limit for the speed loss on the grade.

2.3.3.2 Power to Weight (P/W) Ratio

The user is not expected to input the P/W ratio to the model. Rather, the user will select the most critical (slowest) design vehicle for which the driveway profile will be designed. The P/W ratio will then be determined using the formulae found in the Thomas Gillespie reference, which offers P/W formulas for various type trucks ^(18, p.73). Since the data on which the formulae are based is about 15 years old, the 12.5 percentile formulae are increased by a conservative factor (1.1) approximately equivalent to a time-projected change in the W/P ratio ^(18, p.77 and 17, p.232). Because the P/W ratio of trucks has been increasing over time, this should approximate the less powerful of the trucks (12.5% percentile) on the road today.

Trucks (SU): P/W = 1.1(3.71-.0343U)/1000Trucks with Trailers(WB-12): P/W = 1.1(2.21-.0122U)/1000

Tractor + trailers(WB-15): P/W = 1.1(3.52-.0339U)/100019.8 m (65 ft) Doubles(WB-18): P/W = 1.1(2.96-.0342U)/1000 Examples of the P/W ratios for different speeds is as follows:

l	J	P/W(tı	rucks) I	P/W(trucks	with trailers)	P/W(tr	actor +)	P/W(dou	ıbles)
<u>mph</u>	<u>km/h</u>	hp/lb	hp/kg	hp/lb	<u>hp/kg</u>	hp/lb	hp/kg	hp/lb	hp/kg
10	16.09	.00370	.00816	.00230	.00507	.00350	.00772	.00262	.00578
25	40.23	.00314	.00692	.00210	.00463	.00294	.00648	.00232	.00512

Translating the above P/W ratios to W/P ratios and comparing them to the AASHTO and ITE references, yields the following ranges:

<u>AASHT</u>	O/ITE	<u>Modified</u>	<u>Gillespie</u>
Lb/hp	kg/hp	<u>Lb/hp</u>	kg/hp
250-300	113.4-136.1	270-470	122.4-213.2

Passenger cars have less power but also much less weight. Examples of the least and most powerful of the passenger cars on the road were taken from a distribution of auto P/W ratios, as found in Edmunds ⁽¹⁹⁾ and shown in the Appendix, and are as follows:

<u>P</u>	<u> </u>	<u>/</u>	<u>P</u>	<u>/W</u>
hp	<u>lb</u>	<u>kg</u>	hp/lb	hp/kg
105	2400	1088.4	.0438	0.0966
275	4000	1814.1	.0688	0.1517

A comparison of the P/W ratios of the passenger cars with the trucks, reveals the expected, that passenger cars have more acceleration power on grades. Hence, there is the opportunity to design much steeper grades for passenger cars than for trucks, keeping in mind the stopping requirements of steep negative grades.

2.3.4 Initial Vehicle Speed

The initial speed is the speed at which the design vehicle enters the grade. With higher initial speeds, longer sustained positive driveway grades can be installed before the speed of the vehicle may be reduced to unacceptable levels (see the discussion below on minimum speeds).

The initial vehicle speed of a vehicle exiting the mainline is primarily a function of the design of the intersection of the main road and the driveway and the speed limit on the main road. The design engineer is in the best position to select an initial vehicle speed, but a minimum value of 15 Km/hr is chosen as the default by the model, as reasoned below.

Those access designs (levels) that present the most difficult situations from the point of view of inducing low initial truck speeds are unsignalized access levels 4 and 5 and access level 6 ^(reference 15). A large semitrailer truck, from a stopped position, making a left turn from the main road into a driveway requires at least 18m (60 ft) to accelerate to a speed of 15 km/h (10 mph) ^(17, p.703-5). For the semitrailer truck to accelerate to a speed of 20 km/h (13 mph), it would require 31m (100 ft). To attain these speeds the driveway

profile must not introduce a positive grade that will cause the vehicle to decelerate. Under this mainline/driveway design condition, the attainment of higher initial truck speeds requires greater distances before the start of a positive grade.

At a distance of 18m from the stopped position, a left turning semitrailer is still partially blocking the left lane of the opposing traffic. If a steep positive grade is introduced at this point, the semitrailer will start to decelerate, thereby blocking the opposing lane for a slightly longer period of time. To reduce the total length of the driveway though, the model introduces a positive grade at a variable point 15m (50 ft) from the edge of the travel way. Negative grades can be introduced sooner; the only factor that the negative grade must accommodate is the possible introduction of a crest curve and its clearance from the edge of travel way or shoulder.

The importance of the initial speed of a truck is highlighted by its influence with both the P/W ratio and speed loss.

2.3.5 Minimum Speed

The minimum speed is defined as the slowest speed that is acceptable on a driveway grade. The minimum speed is also important in determining the critical length of a grade. The difference between the initial speed and the minimum speed reflects the maximum speed loss on a grade, which determines the maximum length of grade (critical length) a design vehicle can climb before its speed decelerates below the minimum speed. The design engineer has the option to input the minimum speed, which is obviously less than or equal to the initial speed. Otherwise, a default value will be selected, as determined in the following text.

AASHTO ^(17, p.242) recommends the installation of truck climbing lanes on roads when volume and speed reductions exceed certain limits. The criterion is based on safety and economic considerations. Both are also important considerations for driveways. But driveways must provide a length and grade that prevents a design vehicle decelerating below a minimum acceptable speed, rather than allowing the vehicle to exceed a predetermined speed reduction. Providing additional lanes for a driveway is not considered essential to allow vehicles to bypass slower moving vehicles, unless the driveway volume conditions warrant the lane.

As the bracketed term of the vehicle speed-loss formula approaches 0 (section 2.3.3.1), it will yield the maximum grade for which a particular P/W vehicle can maintain its initial speed.

$$G_{max} < 100*375(P/W)/U$$

Examples of the maximum grades (G_{max}) where individual P/W design vehicles can maintain their initial speed (U) are as follows:

Table 2.4 Maximum Grades Samples

Maximum G	U		P/W		Vehicle Type
	mph	km/h	hp/lb	hp/km	
9	10	16.09	0.00230	0.00507	trucks with trailers
14	10	16.09	0.00370	0.00816	Trucks
6	15	24.14	0.00223	0.00492	trucks with trailers
9	15	24.14	0.00352	0.00776	Trucks
4	20	32.18	0.00216	0.00477	trucks with trailers
6	20	32.18	0.00333	0.00734	Trucks
3	25	40.23	0.00210	0.00463	trucks with trailers
5	25	40.23	0.00314	0.00692	Trucks

As expected, the lower the initial speed of the vehicle, the higher the P/W ratio, the steeper is the grade on which the vehicle's speed can be maintained.

Under different sustained speeds, the maximum grades for design vehicles would be as follows. But most driveways may not be designed for the higher speeds.

Table 2.5 Maximum Grades By Vehicle Type and Speeds

Design Vehicle	Speed				
	10 mph	15 mph	20 mph	25 mph	
Passenger Car	>14%	>9%	>6%	>5%	
Truck(SU)(*bus the same as truck)	14%	9%	6%	5%	
Tractor-trailer (WB-15)	13%	8%	6%	4%	
Bus	14%	9%	6%	5%	

If the initial speed is as low as 15 km/h, a minimum speed of 7.5km/h (approximately 5 mph) may be permitted. This is not a speed that will be experienced by many vehicles; in fact, it will only reflect the oldest and heaviest vehicles on the road. These vehicles represent the 12.5 percentile of the population. Since a very conservative approach has been taken with the use of the P/W ratio, the representation of these vehicles in the population is very small. Using the vehicle speed-loss formula, examples of the critical length of grade for trucks+trailers are as follows (the length of grade at which the vehicle will stop on the grade is also shown). Although most driveways are less than 100', it is important that limiting lengths are shown for those cases where needed.

Table 2.6 Grade Lengths for Tractor + Trailers

Gmax	U		P/W		Critical Length of Grade			
					Min. Speed of 0 mph		Min. Speed of 5 mph	
	mph	km/h	hp/lb	hp/kg	ft	m	ft	m
14%	10	16.09	0.0035	0.00772	760	230	380	115
15%	10	16.09	0.0035	0.00772	360	110	180	55
16%	10	16.09	0.0035	0.00772	230	70	115	35
14%	25	40.23	0.0029	0.00639	170	52	85	26
15%	25	40.23	0.0029	0.00639	160	49	80	25
16%	25	40.23	0.0029	0.00639	140	43	70	22

The discussion of the minimum vehicle speed was not expected to result in a definitive value, but rather suggest a value that can be used in lower level access cases. For situations other than those specified in the text (access levels 4 and 5 and access level 6 from reference 15), the minimum vehicle speed for a driveway may be much higher than 7.5 km/h (the suggested default value). The design engineer may have reason to set a much higher value (consistent with the initial speed), such as to avoid queues backing onto the mainline. The model uses a default minimum speed of 7.5 Km/hour.

2.4 Selection of Design Conditions

When using the model, the design engineer can specify conditions in its application. Others could exist, but these are thought to represent the most common. The designer has the option of selecting any or all of these conditions. Limitations on the proposed grades are set which will determine the design conditions that are acceptable.

- a) The right-of-way that exists or is to be acquired may be a limiting factor for the distance beyond the edge of shoulder that the driveway can extend. Applying this grade may involve the use of a vertical curve, which would also be within the right-of-way.
- b) If the driveway profile cannot attain the grade of the property within the right-ofway, the maximum grade may be suggested. This would necessarily extend beyond the right-of-way.
- c) There may be situations where conditions require the attainment of the grade of the property at a specific point. The option will be offered to the design engineer to select any distance desired.

The introduction in the model of vehicle operating characteristics on grades, vehicle speed loss, initial and sustained vehicle speeds, and the design of vertical curves, suggests a minimum length of grade for the driveway, before consideration is given to using the model. There is no hard and fast minimum to the length of grade to use for the model, but because the vertical curves extend the driveway at two points of vertical intersection, a minimum driveway length of 50' would seem reasonable for use with the model. Therefore, the modeling approach outlined in Volume I-subtitled Design for the Model would only be considered for driveways greater than 50' in length.

For driveways shorter than 50', the designer must first select a grade for the design vehicle (Table 2.5), and check it against the maximum approach/departure grade change, or the crossover grade change (Table 2.2). The designer must then refer to the tables in Volume II-subtitled Design for Sight Distance Considerations to check the limitations for sight distance. The use of the sight distance approach can actually be used for any length driveway.

2.5 Vertical Curve Design

ASSHTO's recommendation for a vertical curve suggests a "...design that is safe (ample sight distance for the design speed), comfortable in operation (ample clearance for the undercarriage of the vehicle and comfortable for the motorist), pleasing in appearance (a long curve has a more pleasing appearance), and adequate for drainage."

The AutoDRIVE model incorporates only symmetrical parabolic vertical curves for driveways.

2.5.1 Stopping Sight Distance (S)

Stopping sight distance is a crucial control for design of vertical curves.

```
S = 0.278 \text{ U t} + \text{U}^2/[254 \text{ (f} + \text{G)}]
```

Where,

S = stopping sight distance, in meters

U = initial/entering speed, in Km/hr

t = brake-reaction time = 2.5 seconds (recommended by AASHTO)

f = coefficient of friction between tires and roadway (wet pavement)

G = longitudinal grade (e.g., if grade = -6%, G for the above formula will be - 0.06)

The model uses the following 'f' values (based on AASTO Green Book):

```
U = 15 \text{ Km/hr}, f = 0.43; U = 20 \text{ Km/hr}, f = 0.42; U = 25 \text{ Km/hr}, f = 0.41; U = 30 \text{ Km/hr}, f = 0.40; U = 35 \text{ Km/hr}, f = 0.39; U = 40 \text{ Km/hr}, f = 0.38; U = 45 \text{ Km/hr}, f = 0.37; U = 50 \text{ Km/hr}, f = 0.35; U = 55 \text{ Km/hr}, f = 0.34; U = 60 \text{ Km/hr}, f = 0.33; U = 65 \text{ Km/hr}, f = 0.32; U = 70 \text{ Km/hr}, f = 0.31
```

2.5.2 Heights of Driver's Eye and Object

Height of Driver's Eye (h_1)

```
For passenger cars, h_1 = 1.07 m
For trucks or buses, h_1 = 2.4 m
```

Height of Object (h₂)

For all design vehicles, $h_2 = 0.15$ m

2.5.3 Minimum Length of Crest Vertical Curve (Lmin)

The general condition for a crest vertical curve is grade 1 > grade 2 (or $G_1 > G_2$). The obstruction that limits the driver's sight distance is the road surface at some point on a crest vertical curve. The major control for safe operation on a crest vertical curve is the provision of ample sight distance for the vehicle entering speed. The other control is the crest curve length in relation to wheelbase length of the design vehicle to avoid cross-over angle hazard.

The AutoDRIVE model compares the user's entered length of vertical curve with the minimum length (L_{min}) required. That is, if $L_{provided} \ge L_{min}$, the curve design length is okay. Otherwise, the model will warn the user that the length of curve is not appropriate.

For driveway design, L_{min} is the greater of the following two:

```
Condition 1.
```

```
when S < L, L_{min} = A S<sup>2</sup> /{100 [ (2 h_1)<sup>1/2</sup> + (2 h_2)<sup>1/2</sup> ] <sup>2</sup> } when S > L, L_{min} = 2 S - {200 [ (h_1)<sup>1/2</sup> + (h_2)<sup>1/2</sup> ] <sup>2</sup> } / A
```

where,

L_{min} = length of vertical curve, in meters

S = stopping sight distance, in meters

A = $|G_2\% - G_1\%|$ (e.g., if $G_2 = -4\%$ and $G_1\% = +3\%$, A = |-4 - (+3)| = 7)

 h_1 = height of driver's eye, in meters

h₂ = height of object, in meters

Condition 2.

 L_{min} = wheelbase of the design vehicle, in meters

Maximum Cross-Over Angle

If L_{min} is based on condition 2 above, the model computes the cross-over angle as follows:

Maximum cross-over angle = Tan⁻¹ [base clearance / (0.5 wheelbase)]

In the above formula, before using the input base clearance value it is first reduced by 25% to take into account the dynamic oscillation of a loaded vehicle along the vertical axis while traversing a curve at slow speed. That is, the model uses the following modified relation:

Maximum cross-over angle = Tan^{-1} [0.75 base clearance / (0.5 wheelbase)]

Note that in the above relation, for WB-12 and WB-15, wheelbase = maximum (WB1 and WB2) and for WB-18, wheelbase = maximum (WB1, BW2, and BW3).

Cross-Over Angle Due to Grade Combination

The cross-over angle due to combination of grades provided is computed by the model as follows:

Available cross-over angle =
$$\frac{\text{Tan}^{-1}}{\text{((|G_2| - |G_1| - [A L_{provided})/800])}} / 100}$$

The model performs the following check:

If available cross-over angle < maximum cross-over angle, design is OK. Otherwise, a warning is echoed to the user regarding the inappropriate design.

2.5.4 Minimum Length of Sag Vertical Curve (Lmin)

The general condition for a sag vertical curve is grade 1 < grade 2 (or $G_1 < G_2$). The AutoDRIVE model uses the headlight sight distance criterion to compute the minimum required curve length. When a vehicle traverses a sag vertical curve at night, the portion of highway lighted ahead is dependent on the position of the headlights and the direction of light beam. The AASHTO Green Book recommends use of a headlight height of 0.6 meter and a 1 degree upward divergence of the light beam from the longitudinal axis of the vehicle. However, this is valid for open highways only. For driveways, it is assumed that the driver can use high beam light at night to see driveway alignment ahead. The study team field observed (for a few vehicles) the upward divergence angle of high beam light. The angle was observed to be approximately 15 degrees. The AutoDRIVE model uses a conservative value of 11.3 degrees for computing length of a sag vertical curve. The modified equations are:

```
Condition 1.
```

when S < L,
$$L_{min}$$
 = A S² / (120 + 3.5 S)
when S > L, L_{min} = 2 S - [(120 + 3.5 S) / A]

where,

$$L_{min}$$
 = length of vertical curve, in meters
S = stopping sight distance, in meters
A = $|G_2\% - G_1\%|$ (e.g., if $G_2 = -4\%$ and $G_1\% = +3\%$, $A = |-4 - (+3)| = 7$)

Condition 2.

 L_{min} = wheelbase of the design vehicle, in meters

Maximum Approach and Departure Angles

If L_{min} is based on condition 2 above, the model computes the approach and departure angles as follows:

```
Maximum approach angle = Tan<sup>-1</sup> [front clearance / (front overhang)]
Maximum departure angle = Tan<sup>-1</sup> [rear clearance / (rear overhang)]
```

In the above formulae, before using the input front and rear clearance values, they are first reduced by 25% to take into account the dynamic oscillation of a loaded vehicle along the vertical axis while traversing a curve at slow speed. That is, the model uses the following modified relations:

```
Maximum approach angle = Tan<sup>-1</sup> [0.75 front clearance / (front overhang)] Maximum departure angle = Tan<sup>-1</sup> [0.75 rear clearance / (rear overhang)]
```

Approach and Departure Angles Due to Grade Combination

The approach/departure angle due to combination of grades provided is computed by the model as follows:

```
Available approach/departure angle = Tan^{-1} {[G_{critical} - (A L_{provided})/800] / 100}
```

The model performs the following check:

If available approach/departure angle < maximum approach/departure angle, design is OK. Otherwise, a warning is echoed to the user regarding the inappropriate design.

2.5.5 <u>Vertical Grade</u>

In order to determine appropriateness of the input vertical grades, the model performs the following checks:

1. Simulated speed > minimum speed (default minimum speed = 7.5 km/hr)

AND

 In case of crest curve, maximum allowable cross-over angle > available cross-over angle
 In case of sag curve, maximum allowable approach/departure angle > available approach/ departure angle.

If the above conditions are met then the vertical grade selected is appropriate, otherwise the model displays a warning regarding inappropriateness of the grade.

2.5.6 Length of Vertical Grade

For length of vertical grade, the model performs the following checks:

- 1. Length of vertical grade > length of design vehicle
- 2. Simulated speed at the end of grade > minimum speed (default min. speed = 7.5 km/hr)

IF THE ABOVE CONDITIONS ARE MET THEN THE LENGTH OF VERTICAL GRADE IS APPROPRIATE, OTHERWISE THE MODEL DISPLAYS A WARNING REGARDING INAPPROPRIATENESS OF THE GRADE LENGTH.

3. MODEL DEVELOPMENT

AutoDRIVE is a 3D CAD based program that simulates movement of a selected design vehicle on a driveway profile. The program was developed using AutoLISP programming language, and it is written in DOS text (ASCII format) using a suitable text editor. AutoDRIVE operates in AutoCAD environment, and includes the following modules:

- 1. Input Module allows user to enter input variables
- 2. Roadway Module draws roadway based on input variables
- 3. Driveway Module draws driveway grades and inserts vertical curves
- 4. Simulation Module places the design vehicle on driveway and performs simulation
- 5. Output Module computes critical design parameters and displays results

A generic flow chart of the model is presented in Figure 3.1.

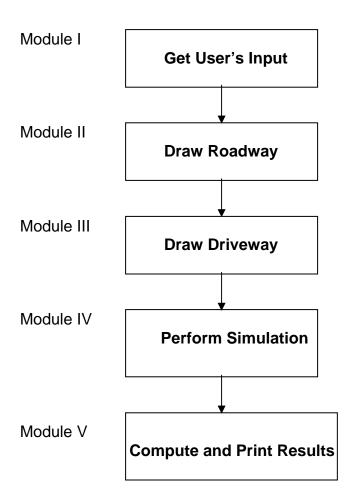


Figure 3.1 Flow Chart of AutoDRIVE Model

3.1 Module I (Input Module)

This module prompts the user to enter the following input parameters:

- Design vehicle. Select the design vehicle from a pop-down menu. A list of design vehicles with their default dimensions (height, length, wheelbase, front overhang, rear overhang, front clearance, base clearance, rear clearance) is provided based on Table II-1 of AASHTO Green Book (17). For example, the user can select P-CAR for passenger car; SU-BUS for single unit bus; SU-TRUCK for single unit truck; and WB-12, WB-15, or WB-18 for truck trailer combinations. The module allows the user to change the dimensions, if desired.
- Entering/initial speed (U) of the design vehicle. The module shows U = 15 Km/hour as the default value. The user can select any initial speed from 15 Km/hr. to 70 Km/hr. with an increment of 5 Km/hr.
- Minimum allowable speed on upgrades of 10 Km/hr. is used as default value.
 The user can enter any other desired minimum allowable speed ranging from 7.5 km/hr 25 km/hr. The model allows to select from the following options:

Minimum speed on upgrade = 7.5, 8, 9, 10, 11, 12, 13, 14, 15, 18, 20, 22, and 25

- Physical elements of roadway. The user can modify default values of:
 - i) Elevation of the outside edge of pavement (m)
 - ii) Total number of roadway lanes in both directions
 - iii) Width of each roadway lane (m)
 - iv) Roadway normal crown cross-slope.
- Physical elements of roadway shoulder and driveway. The user can modify default values of:
 - i) Driveway vertical grade 1 (G₁ in %)
 - ii) Driveway vertical grade 2 (G₂ in %)
 - iii) Length of driveway grade 1 (m)
 - iv) Length of driveway grade 2 (m)
 - v) Roadway shoulder cross-slope
 - vi) Roadway shoulder width (m)
- Lengths of driveway vertical curves. The user can modify default values of:
 - i) Curve length between shoulder and grade 1 (m)
 - ii) Curve length between grade 1 and grade 2 (m)
 - iii) Curve length between grade 2 and property line grade (m)

3.2 Module II (Roadway Module)

This module draws the roadway based on user's input information. These functions are performed in the following sequence:

- **Set the drawing limits.** Based on the input values, this module first defines the drawing limits, and then changes the zoom to drawing limits.
- Draw the roadway. Based on the input information, draws the roadway in 3D.

3.3 Module III (Driveway Module)

This module draws the driveway based on user's input information. These functions are performed in the following sequence:

- **Draw the driveway surface.** Based on the input values of G₁, G₂, lengths of grade1 and grade 2, length of vertical curve, and elevation of the start point, the module draws a 3D driveway surface.
- Place the design vehicle on the driveway surface. The module creates a block
 of the design vehicle and places it on the driveway by making the vehicle tires
 tangent to the driveway surface.

3.4 Module IV (Simulation Module)

This module performs the following functions:

- Move the Vehicle. Simulates the movement of the vehicle on the driveway profile.
 The user can view the simulation in a plan or profile viewpoint. Each time, the
 vehicle is moved by 1 meter from its previous position. At every new location,
 vehicle tires remain tangent to the surface.
- Check appropriateness of cross-over, departure, and approach angles.
- Check for Minimum Standards. If the input values don't meet the minimum standards, warn the user and show the minimum design values. This check is performed at the end of a program run.
- Check Appropriateness of Stopping Sight Distance. Advance the vehicle frame by frame to check the appropriateness of the available sight distance.

3.5 Module V (Output Module)

This module reports results of each simulation run.

4. SAMPLE DESIGN PROBLEMS

This chapter presents two sample design examples, which illustrate how the guidelines, methodologies, and model presented in this report can be used in designing and evaluating vertical alignment of driveways. Both design problems are based on hypothetical data assumed for illustration. The step by step procedure of running the AutoDRIVE model is presented in Appendix B (User's Guide).

Design Problem 1

Driveway/Area Type: Residential

Design Vehicle: Passenger car (P-CAR)

Grade 1: +4%
Grade 2: -10%
Length of Grade 1: 25m
Length of Grade 2: 25m
Length of vertical curve: 6m

Entering Speed: 15 Km/h

The rest of the input parameters including design vehicle dimensions and roadway cross-section details are shown in Figure 4.1 and Table 4.1.

Design Problem 2

Driveway/Area Type: Bus terminal

Design Vehicle: Single unit bus (SU-BUS)

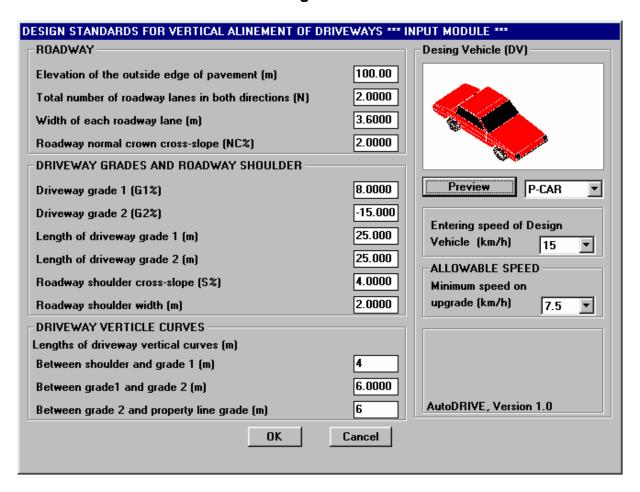
Grade 1: -6%
Grade 2: +11%
Length of Grade 1: 20m
Length of Grade 2: 30m
Length of vertical curve: 10m
Entering Speed: 25 Km/h

The rest of the input parameters including design vehicle dimensions and roadway cross-section details are shown in Figure 4.3 and Table 4.3.

Design Requirements

An evaluation of the appropriateness of the selected design parameters for driveway profile.

4.1 Design Problem 1



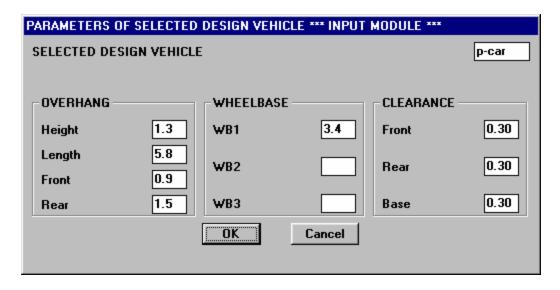


Figure 4.1 Input Data for Design Problem 1

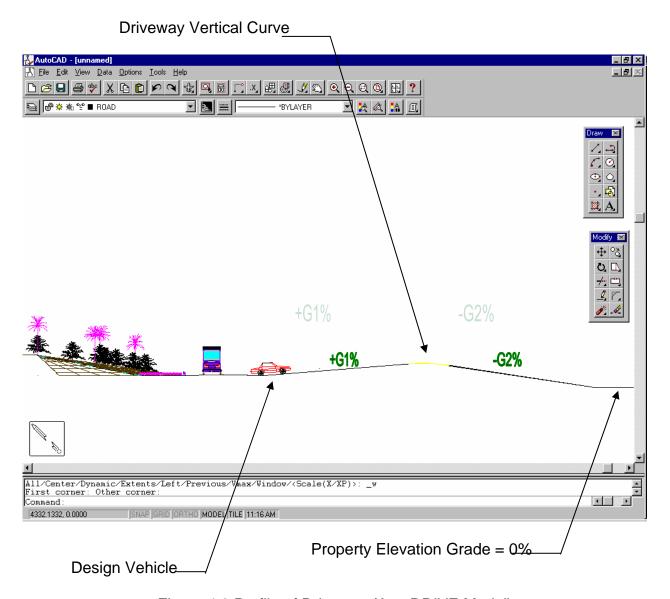


Figure 4.2 Profile of Driveway (AutoDRIVE Model)

Simulation Results (Design Problem 1)

The AutoDRIVE model, after performing design vehicle movement animation, computes all critical design parameters based on criteria established in Chapter 2. The model gives echo of input parameters and simulation output results, which are presented in Tables 4.3 and 4.4, respectively.

Table 4.1 Input Parameters (Design Problem 1)

	Echo of Input Variables								
	Input Parameter								
	Description	Input							
1	Design Vehicle (DV) *	P-CAR							
2	DV entering speed (Km/h)	15							
3	Driveway Grade 1 (G1%)	4							
4	Driveway Grade 2 (G2%)	-10							
5	Length of Grade 1 (m)	25							
6	Length of Grade 2 (m)	25							
7	Length of curve between G1 & G2 (m)	6							
8	Elevation of outside pavement edge (m)	100							
9	Number of roadway lanes in both directions	2							
10	Road lane width (m)	3.6							
11	Roadway cross-slope (NC%)	2							
12	Roadway shoulder width (m)	2							
13	Roadway shoulder cross-slope (S%)	4							
14	Length of curve between shoulder & G1 (m)	4							
15	Length of curve between G2 and property grade (m)	6							
16	Minimum allowable speed on upgrades (Km/h)	7.5							

^{*}P-CAR, SU-BUS, SU-TRUCK, WB-12, WB-15, WB-18

Design Vehicle (P-CAR) Dimensions

Length	FO	RO	WB1	WB2	WB3	FC	BC	RC
5.80	0.90	1.50	3.40	0.00	0.00	0.30	0.30	0.30

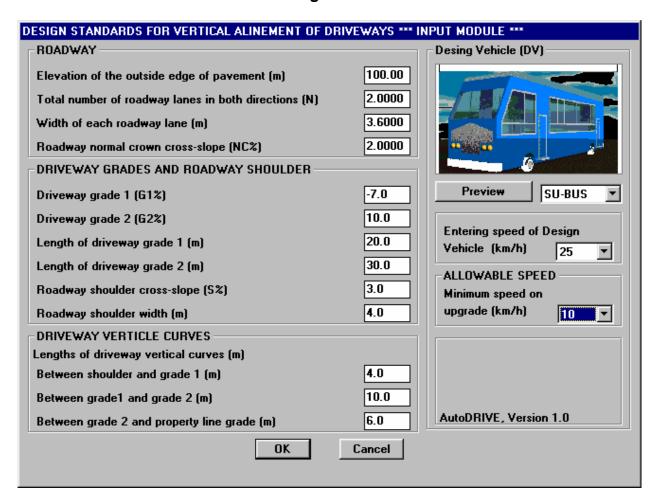
FO = Front Overhang, RO = Rear Overhang, WB = Wheelbase, FC = Front Clearance, BC = Base Clearance, RC = Rear Clearance

Table 4.2 Model Results (Design Problem 1)

	Simulation Output	
	Description	Output
1	Simulated speed at the end of Grade 1 (Km/h)	15.00
2	Simulated speed at the end of Grade 2 (Km/h)	15.00
3	Maximum allowable approach angle (degrees)	Crest Curve
4	Maximum allowable cross-over angle (degrees)	8.53
5	Maximum allowable departure angle (degrees)	Crest Curve
6	Grade combination approach/departure angle (degrees)	Crest Curve
7	Grade combination cross-over angle (degrees)	7.91
8	Stopping sight distance required (m)	12.31
9	Length of curve between G1 & G2 is OK (Y/N)	Υ
10	Length of curve between shoulder & G1 is OK (Y/N)	Υ
11	Length of curve between G2 & property elev. Grade is OK (Y/N)	Υ
12	Grade 1 is OK (Y/N)	Υ
13	Grade 2 is OK (Y/N)	Υ
14	Length of Grade 1 is OK (Y/N)	Υ
15	Length of Grade 2 is OK (Y/N)	Υ

The above results indicate that the design parameters selected for the driveway profile are appropriate and meet all the established designed standards. The designer can perform another test run by selecting more liberal design parameters.

4.2 Design Problem 2



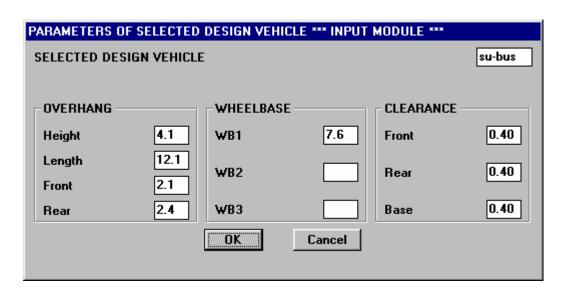


Figure 4.3 Input Data for Design Problem 2

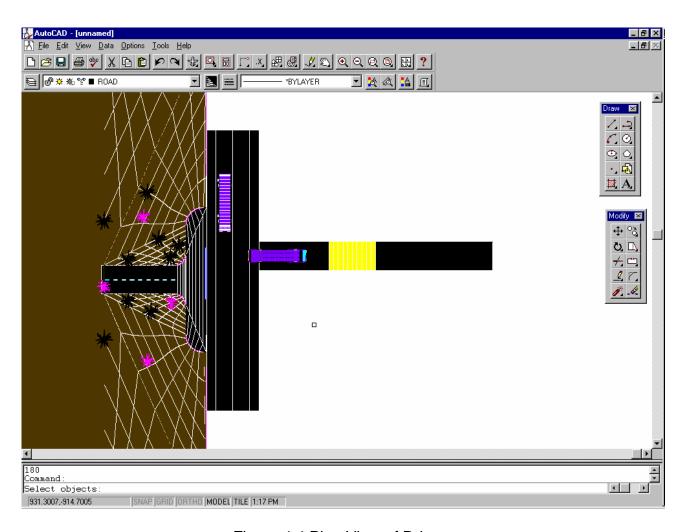


Figure 4.4 Plan View of Driveway

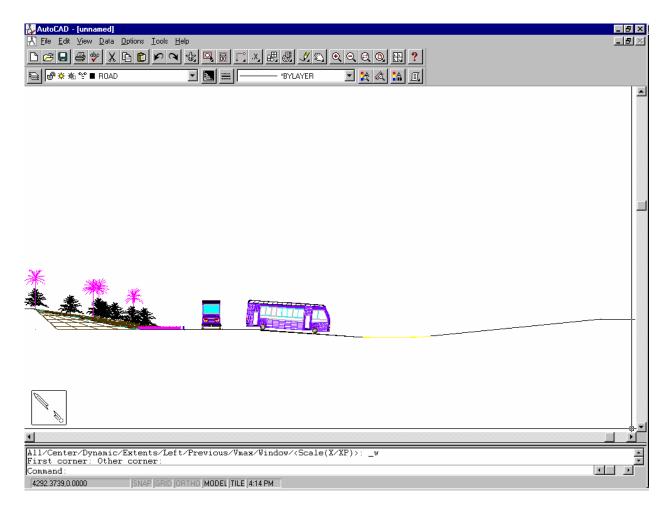


Figure 4.5 Profile of Driveway

Simulation Results (Design Problem 2)

The AutoDRIVE model, after performing design vehicle movement animation, computes all critical design parameters based on criteria established in Chapter 2. The model gives echo of input parameters and simulation output results, which are presented in Tables 4.3 and 4.4, respectively.

Table 4.3 Input Parameters (Design Problem 2)

	Echo of Input Variables								
	Input Parameter								
	Description	Input							
1	Design Vehicle (DV) *	SU-BUS							
2	DV entering speed (Km/h)	25							
3	Driveway Grade 1 (G1%)	-6							
4	Driveway Grade 2 (G2%)	11							
5	Length of Grade 1 (m)	20							
6	Length of Grade 2 (m)	30							
7	Length of curve between G1 & G2 (m)	10							
8	Elevation of outside pavement edge (m)	100							
9	Number of roadway lanes in both directions	2							
10	Road lane width (m)	3.6							
11	Roadway cross-slope (NC%)	2							
12	Roadway shoulder width (m)	2							
13	Roadway shoulder cross-slope (S%)	4							
14	Length of curve between shoulder & G1 (m)	4							
15	Length of curve between G2 and property grade (m)	6							
16	Minimum allowable speed on upgrades (Km/h)	7.5							

Design Vehicle Dimensions

Length	FO	RO	WB1	WB2	WB3	FC	BC	RC
12.10	2.10	2.40	7.60	0.00	0.00	0.37	0.37	0.37

Table 4.4 Model Results (Design Problem 2)

	Simulation Output									
	Description	Output								
1	Simulated speed at the end of Grade 1 (Km/h)	34.80								
2	Simulated speed at the end of Grade 2 (Km/h)	31.20								
3	Maximum allowable approach angle (degrees)	7.53								
4	Maximum allowable cross-over angle (degrees)	Sag Curve								
5	Maximum allowable departure angle (degrees)	6.60								
6	Grade combination approach/departure angle (degrees)	6.16								
7	Grade combination cross-over angle (degrees)	Sag Curve								
8	Stopping sight distance required (m)	24.41								
9	Length of curve between G1 & G2 is OK (Y/N)	Υ								
10	Length of curve between shoulder & G1 is OK (Y/N)	Υ								
11	Length of curve between G2 & property elev. grade is OK (Y/N)	Υ								
12	Grade 1 is OK (Y/N)	Υ								
13	Grade 2 is OK (Y/N)	Υ								
14	Length of Grade 1 is OK (Y/N)	Υ								
15	Length of Grade 2 is OK (Y/N)	Υ								

The above results indicate that the design parameters selected for the driveway profile are appropriate and meet all the established designed standards. The designer can perform another test run by selecting more liberal design parameters.

5 FINDINGS

Procedures have been developed to determine the permissible grades on driveways using a simulation model (Vol. I). Within the model, the grades are dependent on the type of vehicle, length of grade, and the speed of the vehicle entering the grade. The conditions of design for each situation will determine the allowable grades to be used for the driveway, which may exceed the suggested guidelines from the ITE publication⁽⁹⁾.

The more liberal use of design standards can apply to the lower speeds of vehicles that exist on driveways. Lower grades can permit grades to meet at points of intersection, rather than providing vertical curves. The limitation to the intersecting grades is based on the approach/departure and crossover angles of the design vehicle. If steeper intersecting grades are required, the design of a vertical curve is provided.

6. FUTURE RESEARCH

The study of driveway design is a complicated procedure that needs careful consideration of the driveway geometric characteristics, vehicle operation characteristics, and other relevant issues such as the combination of curves in the grade design procedure. The use of computer simulation techniques in the study of grade design provides an important approach to similar studies in the future. Through the accumulation of simulation experience, computers can be better used in future studies of driveway designs. The following issues are suggested for future studies:

In addition to a driveway perpendicular to the roadway, other more complicated driveway geometry needs to be included. The following cases are suggested to be addressed specifically:

- Use a driveway profile that will reach the grade of the property within the existing right-of-way (ROW).
- Use a driveway profile that will reach the grade of the property using maximum possible grade.
- Use a driveway profile that will reach the grade of the property at a selected distance outside the ROW.

The issues related to the combination of horizontal curves and grades need to be considered, because some driveways do not proceed perpendicular from the edge of the main road to the property.

Vertical curve design on grades is important because, they provide ample sight distance, clearance for the undercarriage of the vehicle and comfortable operating conditions for the motorists, as well as pleasing appearance of driveways. However, the combination of vertical curves in the driveway design procedure is a difficult issue that requires study and large-scale data collection and calibrations nationwide. In this study the design of vertical curves on grades follows the AASHTO standards, which is suitable only for roadways. In future studies, vertical curve standards need to be established specifically for driveways.

When a vehicle is moving on a driveway, the suspension of the vehicle varies with both the geometric characteristics of the driveway and the speed of vehicle. The change of suspensions of a moving vehicle leads to the change of cross-over, approach and departure angles, which are critical in the design of vertical grades. The cross-over, approach and departure angles of a moving vehicle, is significantly different from those of a stopped vehicle. In this study, a fixed scale factor is used to adjust the clearance of a moving vehicle. In future studies, moving vehicle suspensions need to be more carefully studied so that the adjustment of the clearance is more accurate.

The formulas of power to weight ratio do not include the formula for buses. Although, there is the opportunity to design much steeper grades for passenger cars than for trucks, a P/W ratio formula for buses needs to be developed in future studies.

The current simulation model is an iterative procedure. Although transportation engineers and planners can run the simulation model iteratively to come up with the best driveway design, it would be more convenient to have a model that is able to assist them automatically to choose a design by revising the current iterative model to a optimization model. This work is left to the future study.

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APPENDIX A

AutoDRIVE Installation Instructions

AutoDRIVE for AutoCAD Version 1.0

Installation Instructions

This manual contains instructions for installation of AutoDRIVE on a personal computer (PC). The subsequent instructions are valid for AutoCAD Versions 12.0 and 13.0. For details on using AutoDRIVE, see Appendix C.

Installing AutoDRIVE

Step 1. Create the following subdirectory for program files:

C:\AUTODRIVE

Windows users:

a) Click on the right side of Address Bar (down arrow) of Windows Explorer and change the drive to C:\. Refer to Figures A-1 and A-2.

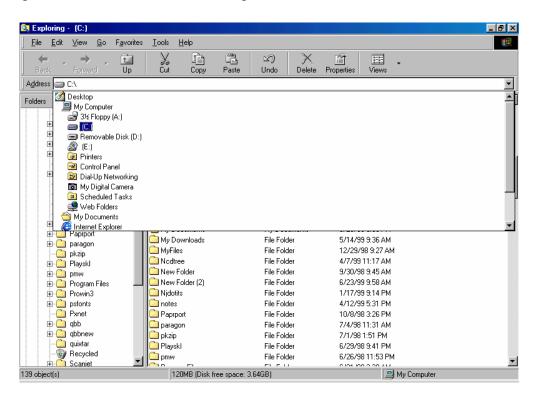


Figure A.1 Using Windows Explorer

b) Click on File (Windows Explorer), place the mouse cursor on New, click on Folder

c) Type AUTODRIVE (see Figure A-2), press Enter

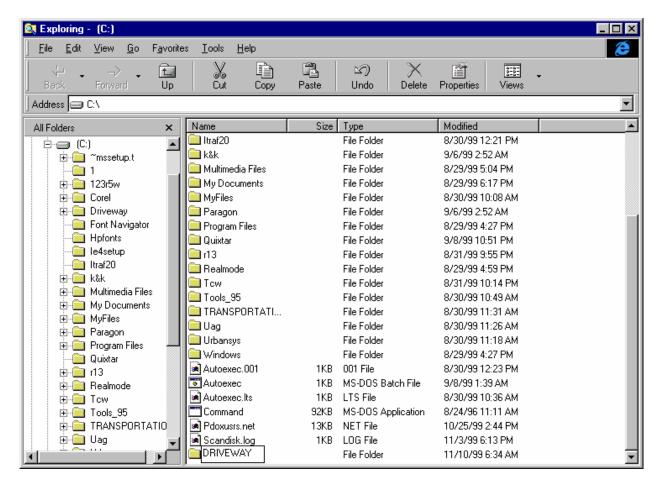


Figure A.2 Creating DRIVEWAY Folder

Step 2. Copy the files from Disk 1 folder of AutoDRIVE CD to the new subdirectory.

Windows users:

- a) Insert AutoDRIVE CD in the CD Rom.
- b) Use Windows Explorer to highlight all files on Disk 1 folder of the CD. This (highlighting of the files) can be accomplished by, first, clicking on the first (top most) file of Disk 1 folder. Next, press the shift key and click on the last (bottom most) file, simultaneously.
- c) Click on the copy icon of Windows Explorer
- d) Double click on C:\AUTODRIVE folder and click on the paste icon of Windows Explorer

Step 3. Copy the files from the AUTODRIVE CD, Disk 2 folder to the AutoCAD support directory (e.g., C:\ACAD13\WIN\SUPPORT or C:\ACAD13\COM\SUPPORT).

APPENDIX B

AutoDRIVE User's Guide

AutoDRIVE for AutoCAD Version 1.0

Introduction

This manual contains step by step instructions for using AutoDRIVE on a personal computer (PC). The subsequent instructions are valid for AutoCAD Versions 12.0 and 13.0.

Using AutoDRIVE

Step 1. Start AutoCAD.

Step 2. Load AutoDRIVE

- a) From the main menu bar, click on TOOLS
- b) Click on APPLICATIONS. The Applications Box shown in Figure C-1 will be displayed.
- c) Click on FILE
- d) Select project1.lsp from the Support subdirectory (For example: c:\acad13\com\support or c:\acad13\win\support)
- e) Select project2.lsp
- f) Select project3.lsp
- g) Select project4.lsp
- h) Select result.lsp
- i) After the above lisp files are listed, select and highlight all the files by a click of the mouse.
- j) Click on LOAD (see Figure B-1)

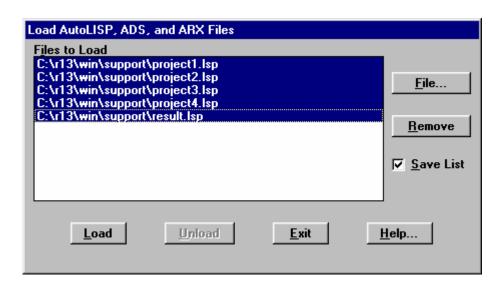


Figure B.1 Loading AutoDRIVE Lisp Files from AutoCAD Applications Box

Step 3. Set 3D View Point

The default 3D Viewpoint setting in AutoCAD is the Plan View. For displaying the vertical profile of the driveway, proceed as follows:

Setting 3D Viewpoint from the Main Menu

- a) Click on VIEW
- b) Place the cursor on 3D Viewpoint Preset
- c) Click on FRONT

Setting 3D Viewpoint Manually

- a) At the command prompt type: ddvpoint and hit Enter i.e. command: ddvpoint <Enter>
- b) Autocad will display the Viewpoint Presets box. Make the following changes:

From: X<u>A</u>xis: <u>2700</u> XY <u>P</u>lane: <u>0.0</u>

c) Click OK (see Figure B-2)

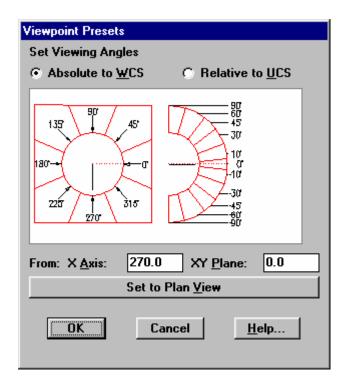


Figure B.2 Setting 3D Viewpoint Manually AutoCAD DDVPOINT Variable

Step 4. Load the Input Module

At the command prompt type project1 (i.e. Command: project1 <ENTER>). The AutoDRIVE will load the input Module as shown in Figure B-3.

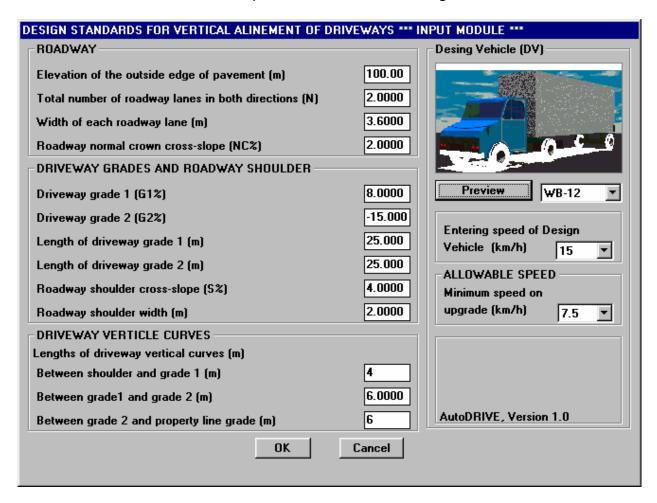


Figure B.3 AutoDRIVE Input Module Box

Input Module

The Input Module box has three subboxes:

1. ROADWAY

The user can alter the elevation of the outside edge of pavement (m). The default value is 100.00 m. Other values in this subbox (e.g., total number of lanes, lane width and the normal crown cross slopes) if altered will not have any effect. This version of AutoDRIVE does not utilize any changes to these values in the calculation/simulation.

2. DRIVEWAY GRADES AND ROADWAY SHOULDER

User can alter any of the input values in this subbox.

3. DRIVEWAY VERTICAL CURVES

- a) Curve between shoulder and G1.
- b) Curve between G1 and G2.
- c) Curve between G2 and Property line grade.

4. **DESIGN VEHICLE**

- a) From the top-down arrow, select the design vehicle.
- b) The user must click on preview to see a 3D display of the selected design vehicle and to be able to edit vehicle dimensions in a subsequent input window box.
- c) Click OK.

5. **DESIGN VEHICLE DIMENSIONS**

- The user can choose one of the following vehicle types:
- Passenger car (P)
- Single unit truck (SU)
- Truck tractor-semitrailer combination (WB-12)
- Truck or truck tractors with semitrailers in combination with full trailers (WB-15 and WB-18)
- Bus (BUS)

For each type of vehicles, there is a set of default dimensions. The model allows the user to edit/modify the dimensions.

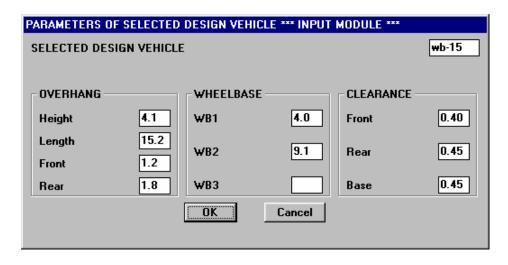


Figure B.4 AutoDRIVE Input Module Box for Vehicle Dimensions

Step 5. Draw the Roadway and Driveway 3D Surface

- a) Type Command: project2 <Enter>
- b) The model draws roadway surface based on input information (see Figure B-5).
- c) The AutoDRIVE will display: Press enter to continue...<Enter>

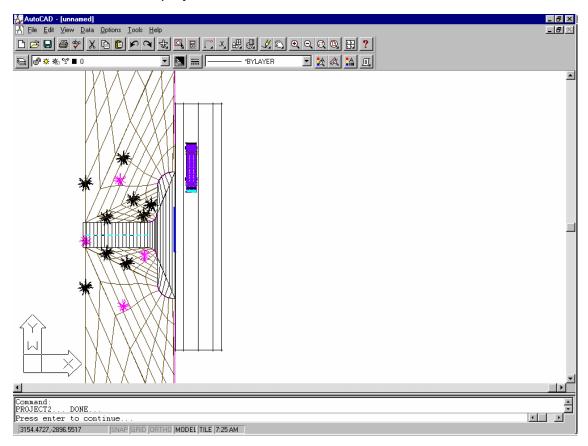


Figure B.5 Project2.lsp Draws the Roadway Surface

Step 6. Draw the Driveway 3D Surface

a) At the Command Prompt, type project3. That is, Command: project3 <Enter>
The AutoDRIVE will plot the driveway surface based on input information (see Figure B-6)

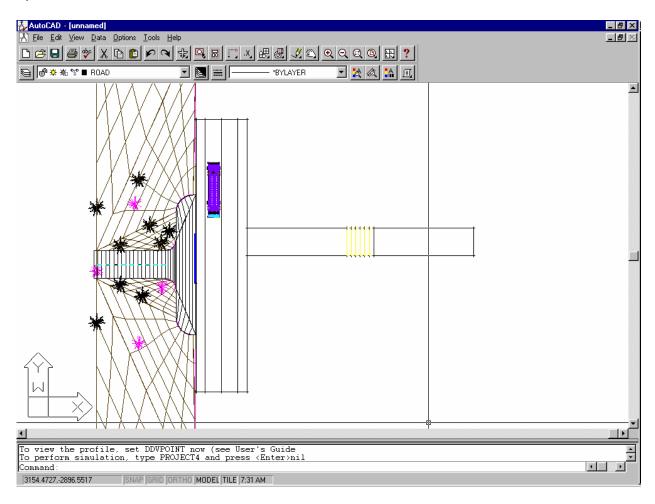


Figure B.6 Project3.lsp Draws the Roadway Surface

Step 7. Simulate Movement of Design Vehicle on Driveway Surface

- a) Type Command: project4 <Enter>
- b) AutoDRIVE will prompt: Select Objects: <Enter>
- c) User will be asked: Press enter to continue ... <Enter>

AutoDRIVE will display the animation of the design vehicle movement on the driveway surface (see Figures 4.4 and 4.5).

APPENDIX C

Field Measurement of Vehicle Clearances

Vehicle clearances are critical to driveway design, because approach, departure and corss-over angles are calculated based on vehicle clearances. Although AASHTO lists dimensions of several vehicle types, there practical limits in measuring clearances on vehicles. A field study was conducted to collect front overhangs, rear over hangs, wheelbases, front clearances, rear clearances and wheelbase clearances. Approach, departure and cross-over angles were calculated based on these information. The collected information were grouped to vehicle types, including passenger cars, tractors and trailers and single unit trucks. Approach, departure and cross-over angles of buses were obtained from web sites of several bus manufacturers.

Table C.1 Field Measurements of Critical Dimensions (Passenger Cars)

	Vehicle Type	Front	Front	Rear	Rear	Wheelbase	Wheelbase	Approach	Departure	Crossover
		Overhang	Clearance	Overhang	Clearance	(m)	Clearance	Angle	Angle	Angle
		(m)	(m)	(m)	(m)		(m)	(degree)	(degree)	(degree)
1	Compact	0.85	0.3	0.95	0.4	2.74	0.27	33.9	39.9	19.5
2	Compact	0.7	0.24	0.73	0.27	2.71	0.18	33.0	35.4	13.2
3	Compact	0.85	0.24	1.01	0.37	2.32	0.24	27.5	35.1	20.4
4	Compact	0.85	0.24	1.04	0.4	2.68	0.24	27.5	36.7	17.7
5	Compact	0.85	0.24	1.1	0.37	2.68	0.24	27.5	32.4	17.7
6	Compact	0.7	0.21	0.98	0.27	2.47	0.21	29.1	26.9	16.8
7	Compact	0.98	0.49	0.98	0.27	2.56	0.18	46.4	26.9	14.0
8	Compact	0.88	0.24	0.85	0.3	2.59	0.24	26.6	33.9	18.3
9	Compact	1.13	0.37	1.01	0.27	2.68	0.24	31.6	26.1	17.7
10	Compact	0.85	0.24	1.07	0.27	2.56	0.21	27.5	24.7	16.3
11	Compact	1.01	0.24	1.01	0.27	2.59	0.24	23.3	26.1	18.3
12	Compact	1.01	0.24	0.79	0.37	2.65	0.24	23.3	43.8	17.9
13	Compact	1.04	0.24	0.73	0.34	2.5	0.21	22.7	43.6	16.6
14	Compact	0.85	0.18	1.04	0.27	2.65	0.24	20.9	25.4	17.9
15	Compact	0.85	0.18	0.98	0.3	2.62	0.18	20.9	29.7	13.7
16	Compact	1.01	0.21	1.19	0.34	2.8	0.24	20.5	27.8	17.0
17	Compact	0.91	0.27	1.19	0.24	2.56	0.24	28.8	19.9	18.5
18	Compact	0.98	0.18	0.98	0.3	2.38	0.21	18.2	29.7	17.5
19	Intermediate	0.73	0.3	0.91	0.37	2.9	0.24	39.0	38.6	16.4
20	Intermediate	0.98	0.4	1.04	0.4	2.38	0.24	38.8	36.7	19.9
21	Intermediate	0.98	0.37	1.07	0.4	2.59	0.24	36.1	35.8	18.3
22	Intermediate	0.98	0.4	1.13	0.4	2.65	0.21	38.8	34.0	15.7

Table C.1 (Continued)

_i abic	C. I (Continue)	<i>a)</i>								
23	Intermediate	0.95	0.37	1.16	0.4	2.77	0.24	37.1	33.2	17.2
24	Intermediate	1.01	0.37	1.01	0.34	2.13	0.24	35.1	32.5	22.2
25	Intermediate	0.91	0.3	1.1	0.37	2.84	0.27	31.8	32.4	18.8
26	Intermediate	1.01	0.37	1.19	0.37	2.77	0.24	35.1	30.1	17.2
27	Intermediate	1.01	0.3	1.19	0.4	2.65	0.27	28.9	32.4	20.1
28	Intermediate	0.79	0.27	1.13	0.34	3.05	0.21	32.9	29.2	13.7
29	Intermediate	0.85	0.24	1.16	0.34	2.87	0.21	27.5	28.5	14.5
30	Intermediate	0.95	0.27	1.07	0.3	2.74	0.24	27.7	27.3	17.3
31	Intermediate	0.88	0.24	0.91	0.37	2.62	0.24	26.6	38.6	18.1
32	Intermediate	1.01	0.27	1.19	0.4	2.8	0.27	26.1	32.4	19.1
33	Intermediate	1.07	0.27	1.19	0.4	2.71	0.24	24.7	32.4	17.5
34	Intermediate	0.95	0.37	1.22	0.3	2.71	0.24	37.1	24.1	17.5
35	Intermediate	1.01	0.24	0.98	0.37	2.8	0.27	23.3	36.1	19.1
36	Intermediate	1.28	0.3	1.22	0.4	2.8	0.3	23.0	31.7	21.1
37	Intermediate	1.01	0.21	1.1	0.37	2.74	0.24	20.5	32.4	17.3
38	Intermediate	0.7	0.18	1.16	0.18	2.9	0.18	25.2	15.4	12.4
39	Large	0.73	0.37	0.73	0.46	2.68	0.24	46.9	56.2	17.7
40	Large	0.73	0.4	0.88	0.4	2.65	0.37	50.1	42.7	27.2
41	Large	0.76	0.4	1.16	0.52	2.8	0.34	48.4	42.1	23.8
42	Large	0.88	0.52	1.1	0.43	2.74	0.37	53.4	37.3	26.4
43	Large	0.82	0.4	1.04	0.4	2.68	0.24	45.4	36.7	17.7
44	Large	0.82	0.37	0.98	0.37	2.87	0.27	42.4	36.1	18.6
45	Large	0.88	0.37	1.19	0.4	2.93	0.37	39.8	32.4	24.7
46	Large	1.07	0.4	1.1	0.37	2.74	0.24	35.8	32.4	17.3
47	Large	1.04	0.37	1.16	0.37	2.41	0.24	34.2	30.9	19.7
48	Large	0.95	0.27	0.98	0.37	2.96	0.24	27.7	36.1	16.1

Table C.1 (Continued)

49	Large	0.82	0.24	1.16	0.34	3.11	0.21	28.5	28.5	13.4
50	Large	0.91	0.3	1.28	0.37	3.05	0.27	31.8	28.1	17.5
51	Large	1.16	0.34	1.28	0.37	2.8	0.24	28.5	28.1	17.0
52	Large	1.25	0.37	1.43	0.4	2.87	0.24	28.8	27.3	16.6
53	Large	0.88	0.24	1.4	0.37	3.11	0.27	26.6	25.8	17.2
54	Large	0.82	0.21	0.61	0.3	2.38	0.24	25.1	45.7	19.9
55	Large	0.98	0.37	1.43	0.37	2.99	0.24	36.1	25.3	15.9
56	Large	1.1	0.37	1.43	0.37	2.99	0.24	32.4	25.3	15.9
57	Large	1.01	0.3	1.43	0.37	2.99	0.24	28.9	25.3	15.9
58	Large	1.16	0.37	1.25	0.3	2.96	0.24	30.9	23.6	16.1
59	Large	0.91	0.21	1.28	0.3	2.74	0.24	22.7	23.0	17.3
60	Large	1.16	0.34	1.37	0.3	2.99	0.24	28.5	21.6	15.9

Table C.2 Field Measurements of Critical Dimensions (Tractors and Trailers)

	Vehicle Type	Wheelbase (m)	Wheelbase Clearance (m)	Crossover Angle (degree)
1	Tractor	2.62	0.37	27.5
2	Tractor	3.38	0.37	21.6
3	Tractor	3.84	0.4	20.5
4	Tractor	3.41	0.34	19.7
5	Tractor	5.15	0.43	16.5
6	Tractor	3.69	0.3	16.1
7	Trailor	9.51	0.91	18.9
8	Trailor	7.68	0.73	18.8
9	Trailor	8.23	0.76	18.3
10	Trailor	6.89	0.58	16.7
11	Trailor	10.37	0.85	16.2
12	Trailor	9.97	0.79	15.7
13	Trailor	9.24	0.73	15.7
14	Trailor	9.24	0.73	15.7
15	Trailor	10.98	0.82	14.8
16	Trailor	10.98	0.82	14.8
17	Trailor	11.59	0.85	14.6
18	Trailor	10.88	0.79	14.4
19	Trailor	10.06	0.7	13.8
20	Trailor	9.76	0.67	13.6
21	Trailor	10.76	0.73	13.5
22	Trailor	6.83	0.46	13.4
23	Trailor	10.98	0.73	13.2

Table C.3 Field Measurements of Critical Dimensions (Single Unit Trucks)

	Vehicle Type	Wheelbase (m)	Wheelbase Clearance (m)	, ,		Crossover Angle (degree)	Dept. Angle (m)
1	single unit truck	5.55	0.58	2.59	0.46	20.6	17.6
2	single unit truck	5.12	0.46	2.68	0.49	17.8	18.1
3	single unit truck	4.51	0.37	1.98	0.49	16.3	24.3
4	single unit truck	4.02	0.30	1.71	0.37	14.8	21.3
5	single unit truck	4.45	0.30	1.65	0.37	13.4	22.1
6	single unit truck	3.41	0.21	1.83	0.30	12.3	16.2

Table C.4 Measurements of Critical Dimension (Buses)

	Vehicle Type	Wheelbase		Front Overhang				Approach Angle*	Departure Angle*	Crossover Angle*
		(m)	(inch)	(m)	(inch)	(m)	(inch)	(degree)	(degree)	(degree)
1	NABI Model 416	6.7	264	2.2	86	3.0	118	9	9	10
2	NABI Model 40CFW	7.0	276	2.2	86	3.0	118	9	9	10
4	29' Q-Bus	3.8	151	2.1	81.5	3.0	118.5	8.3	7.9	16.8
5	35' and 37' Q-Bus	5.6	221	2.1	81.5	3.0	118.5	8.5	7.6	10

Source: 1, 2 and 3 http://www.trabsut-cebter,cin/NABI/buses 4, and 5 http://www.blue-bird-com/comm.html
* Suspension factor has been adjusted.